

### SEMI-ANNUAL TECHNICAL REPORT

to the

AIR FORCE OFFICE OF SCIENTIFIC RESEARCH

from

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PHASE-MATCHED FILTERS FOR SELECTED SOURCE-RECEIVER PATHS

Geophysical Laboratory Southern Methodist University Dallas, Texas 75275 28 February 1978

### ABSTRACT

Phase-matched filters have been developed for several paths of interest for both Rayleigh and Love waves. filters are presented in the form of tabled values of apparent group velocity as a function of frequency. Detailed instructions are given as to how the tabled values can be used to construct phase-matched filters and how the filters can be applied to low-level signals which have travelled the same path. Application of the filters provides a time series in which the effects of multipaths have been minimized and on which the signal-to-noise ratio is improved by a factor proportional to the time compression of the signal achieved by the filtering. For a signal bandwidth of 0.1 - 0.015 Hz and an epicentral distance of 30 degrees, the signal-tonoise ratio is about 10 dB better than on the original seismogram. The filtered seismogram can be used for the determination of surface wave magnitude.

#### INTRODUCTION

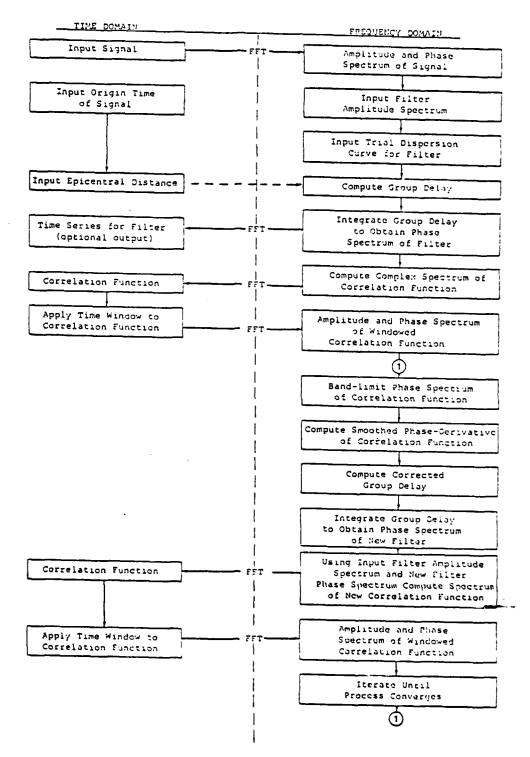
Phase-matched filters have been defined (Herrin and Goforth, 1977) as a class of linear filters in which the Fourier phase of the filter is made equal to that of a given signal.

Consider the Fourier transform of the cross-correlation of a signal, s(t), with a time function, f(t), to be  $S(t) \otimes f(t) \Longrightarrow |S(\omega)||f(\omega)| \exp i G(\omega) - \phi(\omega)|$  Now suppose that we choose fp(t) such that the Fourier phase is the same as that of s(t). We define the class of linear operators, fp(t), such that  $G(\omega) = \beta(\omega)$ , as phase-matched filters with respect to the signal, s(t). The output of the above operation will then have the Fourier transform,  $|S(\omega)||Fp(\omega)|$ , and will be an even function in the time domain as is the autocorrelation function. We call this output a pseudo-auto-correlation function (PAF). If means can be found for matching the Fourier phase of the signal and the filter, then the PAF will depend, for a given signal, only upon the amplitude spectrum of the particular phase-matched filter used in the operation. If  $|Fp(\omega)|$  is chosen to be equal to  $|S(\omega)|$ ,

the phase-matched filter becomes the matched filter and maximizes the signal to noise power ratio assuming "white noise". The PAF becomes the autocorrelation function. At the other extreme, if  $||\mathbf{Fp}(w)||$  is chosen to be  $1/|\mathbf{S}(w)||$ , the PAF becomes the impulse function. In practice, this choice would maximize the time resolution of the output but would greatly reduce the signal to noise ratio. Experience has shown that in the case where the amplitude spectrum is unknown a useful choice for the filter is  $||\mathbf{Fp}(w)|| = 1$ , the "white" filter.

In many cases, seismic signals are composed of two or more components overlapping in time. For example, Rayleigh and Love waves are almost always composed of overlapping wave trains representing multi-path propagation. A first task in the analysis of seismic surface waves is to identify and separate the various component wave trains so that each can be analyzed separately. Herrin and Goforth (1977) described an iterative technique which can be used to find a phase-matched filter for a particular component of a seismic signal. A flow diagram of the technique is shown in Table 1. They applied this process to digital records of Rayleigh waves from an earthquake and an explosion. Application of the filters allowed multiple arrivals to be identified and removed, and allowed recovery of the complex spectrum of the primary wave train and the estimation of the group velocity dispersion curve.

TAU'E 1 FLOW STAGRAM



The amplitude spectrum of the primary signal obtained by this linear process was not contaminated by interference from the multipath arrivals.

The application of phase-matched filtering to Love waves was demonstrated by Goforth and Herrin (1979), and the use of the technique to improve the signal-to-noise ratio of Rayleigh waves was documented by McDonald et al (1974).

This report contains the initial entries of a catalog of phase-matched filters obtained for various paths of interest for both Rayleigh and Love waves. The catalog, which will be augmented in future reports, is in the form of tabled values of apparent group velocity as a function of frequency. group velocity curves are termed apparent because it is not known if the surface wave has travelled a great circle path. Also, the initial phase spectrum of the source has been incorporated into the dispersion curves; the phase response of the seismograph has not been removed; and the group delays from which the dispersion curves are calculated are relative to an arbitrarily assigned signal delay. However, these factors do not affect the use of the phase-matched filters as described in this report. Detailed instructions are given as to how the tabled values can be used to construct phase-matched filters, which in turn can be applied to low-level signals which have travelled the same path.

### DESIGN AND APPLICATION OF THE FILTERS

The tabulated dispersion curves provided in the catalog in the Appendix can be used to design phase-matched filters for the indicated paths. The first step is to calculate the group delay; i. e.,

$$G(f) = \frac{d}{U(f)} - \frac{d}{V_O}$$

where G(f) is the group delay at each frequency in seconds,

- d is the great circle distance in km between the epicenter and the recording station,
- U(f) is the tabulated value of apparent group velocity
   at each frequency, and
- $V_{\rm O}$  is taken to be 4.0 for Rayleigh waves and 4.5 for Love waves.

The term  $\frac{d}{V_0}$  is an arbitrary signal delay which was assumed in determining the apparent group velocity. The integral of the group delay is the Fourier phase of the dispersed wave train; i.e.,

 $\emptyset(f_0) = \int_0^{f_0} G(f)df + C$ 

where C is a constant given for each path and  $\emptyset(f_0)$  is the Fourier phase at  $f_0$  in cycles. The quantity  $\emptyset(f)$  is the phase of the phase-matched filter; the amplitude spectrum of the filter should be specified to be unity to frequencies as high as 0.1 Hz and to roll off sharply at higher frequencies. A recommended amplitude spectrum is shown in figure 1. The phase-matched filter, whose Fourier transform is  $A(f)e^{i\theta}$ , can then be correlated with

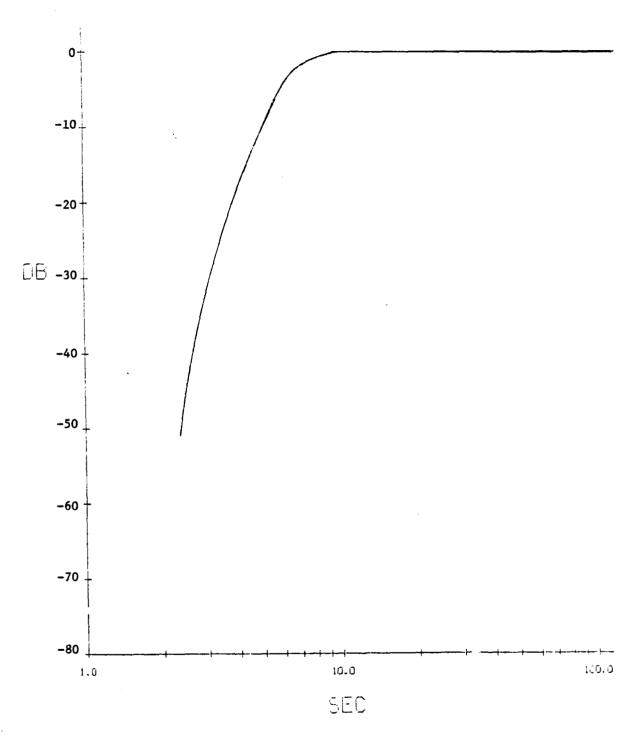


Figure 1. Amplitude spectrum recomme ded for the phase-matched filters.

a surface wave of interest which has travelled approximately the same path. The correlation can be accomplished in the frequency domain by first taking the Fourier transform of the signal. It is convenient to select the arrival time of energy travelling at 4.0 km/sec as the left side of the transform window for Rayleigh waves. A value of 4.5 km/sec is satisfactory for Love waves. A window length of 2048 seconds has been found to be adequate for nearly all signals in the period range 10 to 100 seconds which are sampled once per second. If the Fourier transform of the signal is

$$S(f)e^{i\theta(f)}$$

the correlation function in the frequency domain is

$$C(f) = A(f)S(f)e^{i\varphi(f)} - \emptyset(f).$$

where  $\Psi(f)$  is close to zero in the band of interest. The inverse Fourier transform of  $C(f)e^{i\psi(f)}$  will yield a time domain representation of the correlation function which will have a S/N improvement, relative to the original signal, that is proportional to the time compression of the signal achieved by phase-matched filtering. For a bandwidth of 0.10 to .015 Hz and an epicentral distance of  $30^{\circ}$ , the S/N improvement for seismic surface waves is about 10 dB.

Phase-matched filters offer an advantage over master event matched filtering in that the same filter can be used

over significant deviations in travel path. The phase characteristics of most surface waves are quite strongly influenced by multipathing, and the effects of multipathing are extremely sensitive to small changes in travel path.

Thus, master events, which include multipathing effects, are usually found to be inefficient when applied to slightly different paths. Phase-matched filters are designed to the phase of the primary (first arriving) wave train and exclude the effects on the phase of later arriving composite characteristics of the phase-matched filter are therefore controlled by the average of the earth properties along the path and are not so sensitive to small changes in path.

### APPLICATION OF PHASE-MATCHED FILTERING TO MAGNITUDE DETERMINATION

The Rayleigh waves shown in figure 2 were recorded on the vertical seismograph at the Albuquerque Seismic Research Observatory (SRO). Epicentral information concerning the two earthquakes is given in Table 2. The two events were located near Iceland within 20 kilometers of each other. The Rayleigh wave of event 76-004 (figure 2b) contains interfering body waves from an earthquake in Argentina. The interference is especially noticeable in the portion of the wave in which 20-sec energy is arriving. A magnitude (Ms) determination made by measuring the amplitude at a period of 20 seconds would be in error.

Following the iterative technique diagrammed in Table 1, a phase-matched filter was determined for event 76-033 (figure 2a). The filter was applied to both events; the resulting pseudo-autocorrelation functions (PAFs) are shown in figure 3. A comparison of the PAFs indicates the following; (1) The same filter produces almost identical results on the two signals as should be the case since the epicenters are so close together. Even the multipath structure which trails the peak for about 170 seconds is nearly identical. (2) The Iceland earthquake has been completely resolved from

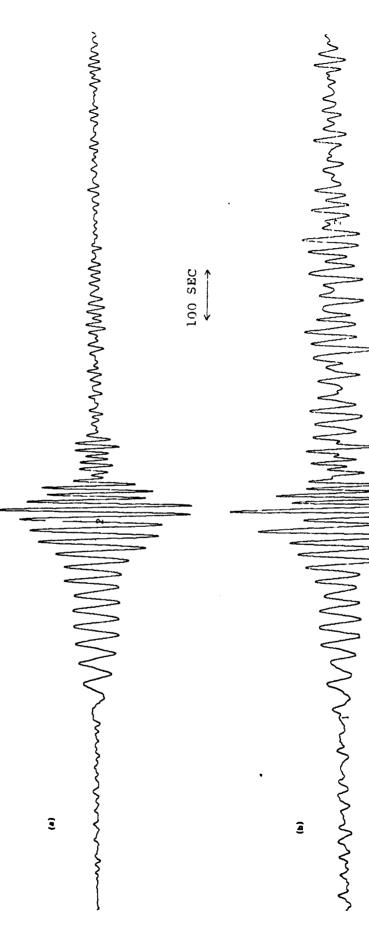
interfering Argentina event by the correlation, and an amplitude measurement, undisturbed by either the low-level multipathing or by the relatively strong Argentina body waves, could be made on the main peak of the PAF. Such a measurement, if accompanied by an empirically-derived relationship between the PAF amplitude and the conventional amplitude at a period of 20 seconds, could be used to calculate a surface wave magnitude from which the effects of multipathing and interfering events have been eliminated. In addition, the measurement would be made on a time series in which the signal-to-noise ratio is approximately 10 dB higher than on the seismogram.

The amplitude of the pseudo-autocorrelation peak is a function of the integral of the signal spectrum. Thus, the PAF peak amplitude is determined not only by the peak spectral amplitude of the signal but also by the frequency bandwidth of the signal. For a given signal peak spectral amplitude, the PAF amplitude will increase with the signal bandwidth. If a relation is established empirically between conventional Ms (at 20 sec) and PAF peak amplitude for explosions, then a magnitude (Mp) determined from the PAF may prove a useful Mp:m discriminant because of the greater bandwidth of earthquake surface waves.

We are developing phase-matched filters for as many paths

as possible and, beginning with the Appendix to this report, we plan to present the data in a format so that anyone interested can construct and use the filters. The epicentral information concerning the seismic events included in the Appendix is given in Table 3.

The phase response of the seismograph has not been removed from the data from which the phase-matched filters can be constructed. Thus, the filters can be applied directly to signals recorded at the Albuquerque and Meshed Seismic Research Observatories. However, the instrument phase response incorporated in the ALPA phase-matched filters is that of the Geotech Triaxial Long-period seismometer. These instruments have recently been replaced by Geotech KS-36,000 seismometers; phase-matched filters applied to ALPA data recorded after the instrument change should be adjusted by the difference in phase response of the seismographs.

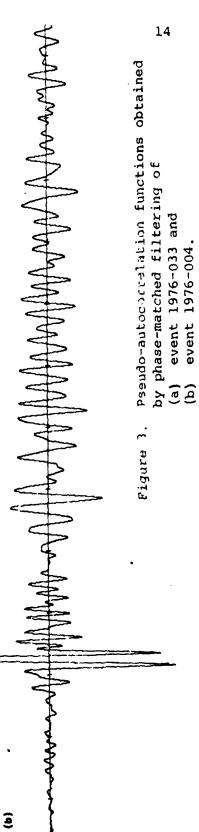


Rayleigh waves from Iceland earth juakes recorded at Albuquerque, N. M. (a) event 1976-033, (b) event 1976-004 Figure 2.

event 1976-004.

PABLE 2

RECORDING SITE	Albuquerque	Albuquerque
DEPTH	33	Ŋ
g <sup>Q</sup>	5.0	4.8 5
DISTANCE	58.558	
LONG	16.688W	16.773W
LAT	66.047N	66.122N
ORIGIN TIME	1976-004-04-29-29.3 66.047N 16.688W 58.558 5.0 33	1976-033-13-16-45.7 66.122N 16.773W 58.504
EVENT	Iceland	Iceland



100 SEC

3

ABLE 3

EVENT	ORIGIN TIME	LAT	LONG	DISTANCE	EΩ	DEPTH	RECORDING SITE
Iceland	1976-004-04-29-29.3	66.047N	16.688W	58.558	5.0	33	Albuquerque
Novaya Zemlya	1975-294-11-59-57.3	73.35N	55.08W	71.28	6.5	0	Albuquergue
Kuril Is.	1976-022-08-07-10.4	44.39N	149.617E	65.83	5.4	44	Meshed, Iran
Andreanof Is.	1974-201-00-48-3.9	51.60N	173.50W	19.03	4.9	45	ALPA
Komandorsky Is.	1975-308-12-05-56.9 54.40N 167.50W	54.40N	167.50W	24.65	5,5	24	ALPA

### REFERENCES

- Goforth, Tom and Eugene Herrin, 1979. Phase-matched filters: Application to the study of Love waves, <u>Bull. Seis. Soc. Amer.</u>, vol. 67, no. 1, February.
- Herrin, Eugene and Tom Goforth, 1977. Phase-matched filters: Application to the study of Rayleigh waves, <u>Bull. Seis.</u> Soc. Amer., vol. 67, no. 5, 1259-1275.
- McDonald, J. A., William Tucker, and Eugene Herrin, 1974.

  Matched filter detection of surface waves of periods up
  to 75 seconds generated by small earthquakes, <u>Bull. Seis.</u>
  <u>Soc. Amer.</u>, vol. 64, 1843-1854.

### APPENDIX

## CATALOG OF GROUP VELOCITY DISPERSION CURVES AND TABLES

1. Kuril Islands - Meshed, Iran (Rayleigh)

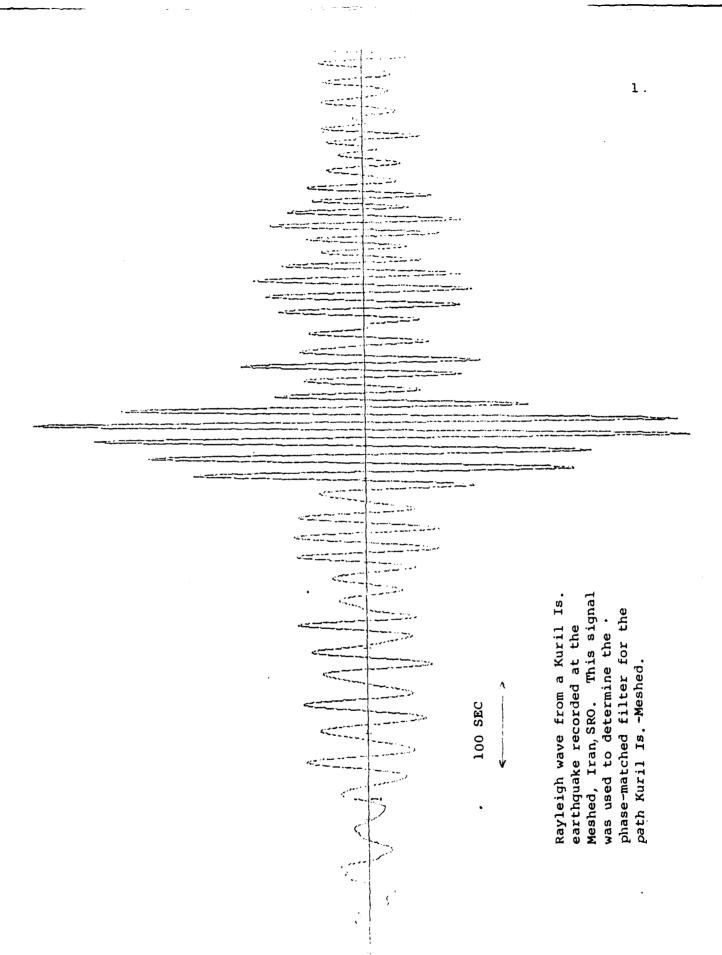
2. Novaya Zemlya - Albuquerque, N. M. (Rayleigh)

3. Novaya Zemlya - Albuquerque, N. M. (Love)

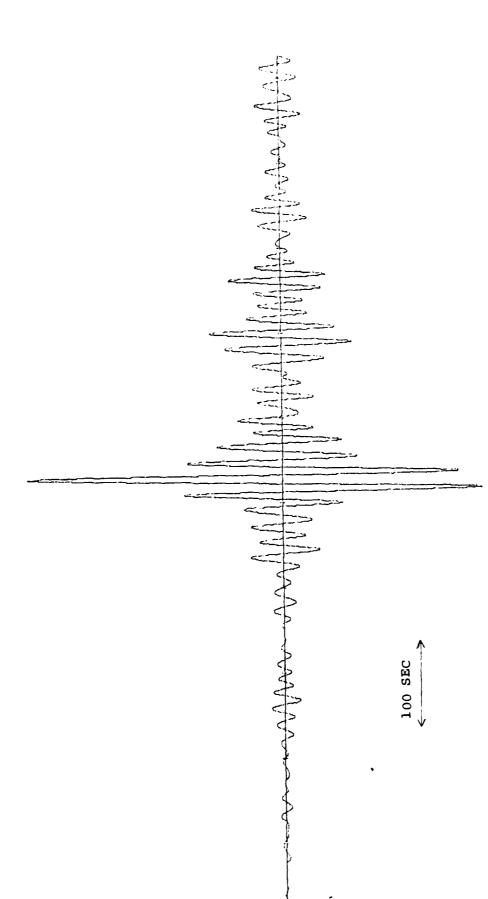
4. Andreanof Island - ALPA (Rayleigh)

5. Komandorsky Island - ALPA (Rayleigh)

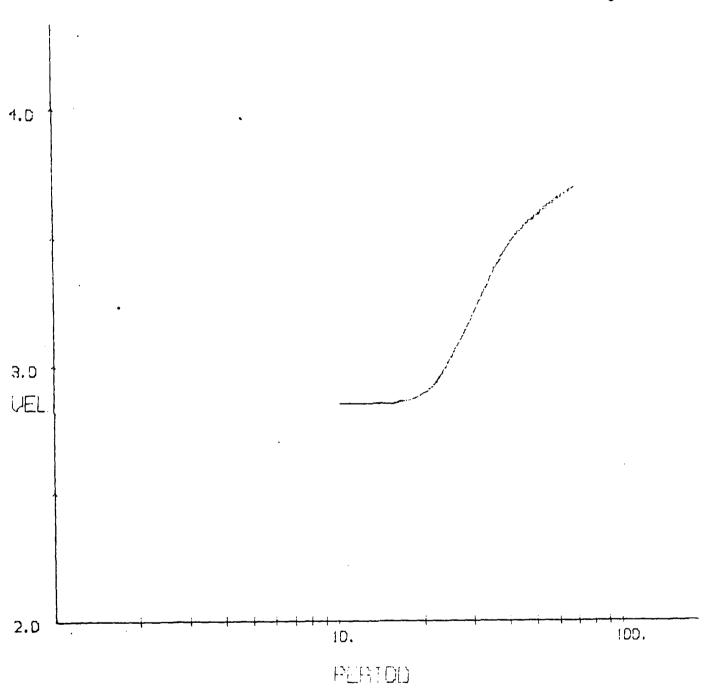
5. Iceland - Albuquerque, N. M. (Rayleigh)



•



The pseudo-autocorrelation function obtained by the application of the Kuril-Meshed phase-matched filter to the Kuril event.



Plot of the apparent Rayleigh group velocity dispersion curve obtained for the Kuril-Meshed path.

(

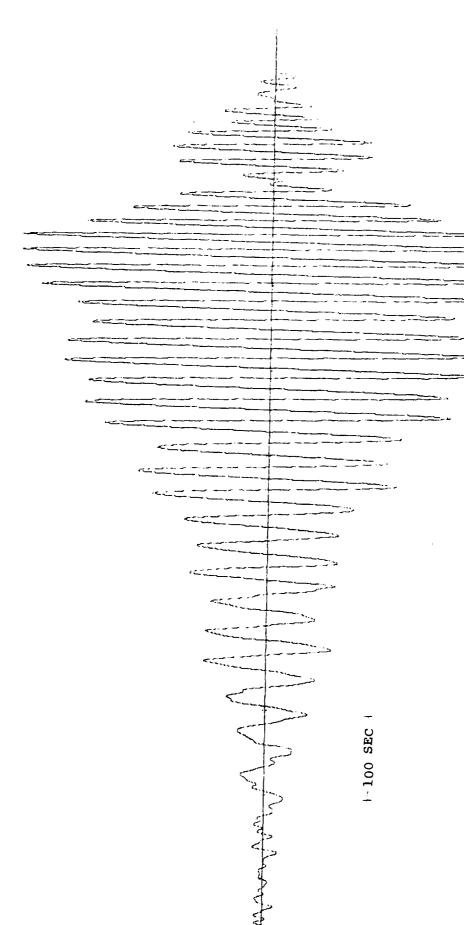
TABLED VALUES OF THE APPARENT RAYLEIGH GROUP VELOCITY DISPERSION CURVE FOR THE PATH KURIL ISLANDS (44.39N, 149.62E) - MESHED, IRAN (36.30N, 59.49E).

KURIL IS. (44.39N, 149.62E) - MESHAD, IRAN (36.30N, 59.49E)C = +0.010 cycles

	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
	•00049	3.9837	•32100	3.5714
	•00098	3 • 9558	• 02148	3.5619
	•00146	3.9187	•02197	3.5521
	•00195	3 • 8755	•02246	3.5421
	•00244	3.8267	•02295	3.5316
	•00293	3.7773	•02344	3.5203
	•30342	3.7303	•05393	3.5395
	•00391	3 • 6 3 9 7	•02441	3.4978
	•00439	3 • 6565	•02490	3.4842
	•00488	3.6506	•02539	3.4698
	•00537	3 • 6 5 8 9	•02538 .	3 • 45 49
	•30586	3.6735	•02637	3 • 4 3 9 8
	·00635	3.6974	•02636	3 • 4243
	•00634	3.7127	•02734	3 • 4086
	•00732	3.7249	•02783	3.3926
	•00781	3.7310	•02832	3.3766
	•00830	3.7354	•02861	3.3504
	•00879	3 • 7383	•02930	3.3442
	•30928	3.7397	•02979	3.3282
	•00977	3.7405	•03027	3.3124
	•01025	3.7412	•03076	3.2965
	•01074	3.7409	•03125	3.5806
	•01123	3.7397	•03174	3.2653
	•01172	3.7375	•03883	3.2499
	15510•	3.7339	•03271	3.2346
	•01270	3.7291	•03320	3.2195
	•01318	3.7232	•03369	3.2347
1	•01367	3.7165	•03418	3.1900
L	•01416	3.7092	•03467	3 • 1758
	•01465	3.7)12	•03516	3.1251
	•01514	3.6023	• 33564	3 • 1 + 8 6
	•01503	3.6329	•03613	3 • 135 4
	•01611	3 • 6 7 3 1	•03662	3.1224
	•01660	3 • 6531	•03711	3.1097
	•01709	3.6528	•03760	3.0973
	•01758	3.6423	•03809	3.0851
	·018J7	3.6315	•03857	3.0732
	•01855	3.6203	•039.)6	3.0616
	•01904	3.6399	•03955	3.0502
	•01953	3.5991	•04004	3.0387
	•02002	3.5900	•04053	3.0274
I .	•02051	3.5368		3.5165

FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
•04150	3.0060	•06348	2.8501
•04199	2.3958	•06396	2.8593
•04248	2.9360	•06445	2.8537
•04297	2.9767	•06494	2 • 8586
•04346	2.9578	• 06543	2.3586
•04395	2.9593	•06592	2.8388
•04443	2.9514	•06641	2.8590
•04492	2.9448	•06669	2.8593
•04541	2.9389	•06738	2.8395
•04590	2.9333	•06787	2.8600
•04639	2.9583	•06836	2 • 8 5 0 4
•04688	2.9735	•06885	2.8609
• 347.36	2.9193	•06934	2.8513
•04785	2.9152	•06982	2.8517
• 0 4 8 3 4	2.9115	•07031	2.3620
• 04833	2.9781	•07060	2.8523
•0+932	2.9749	•07129	2 • 3525
•04930	2.9017	•07178	2.8630
•05029	2.8786	•07227	2.8634
•0507ä	2.8955	•07275	2.8634
•05127	2.8928	•07324	5.3200
•05176	5.9905	•07373	2.8600
•05 <b>2</b> 25	2.8878	•07422	2.8603
•05273	2 • 8356	•07471	2.3500
•05322	2 • 3 5 3 5	•07520	2.3600
•05371	2.8216	•07568	2.8600
•05420	2 • 8798	•07617	2.8500
•05469	2.8783	•07666	2.8500
•05518	2 • 3769	•07715	2 • 8 5 0 0
• 05566	2.3	•07764	2.8500
•05615	2 • 8745	•07813	2.8500
•05664	2 • 8734	•07861	2.8600
•05713	2.8725	•07910	2.3500
•05762	2.8715	•07959	2.3500
•05811	2.8707	•08003	2.3500
• 35859	5 • 36 50	• 23057	3 • 3603
•05908	2.9935	•03105	2.8500
•05957	2 • 3584	•03154	2.8500
•36006	2 • 8672	•08203	2.8600
•36055	2.8661	•08252	2.8500
•36104	2 • 3649	•08301	2.3500
•06132	2.3538	•08350	C098.2
•36231	2.8628	•08398	2.8600
•06250	2.8618	•08447	5 • 8600
•36299	2.8509	•38496	Z•85JD.

FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
•085+5	2.3500
•0.3594	2.8500
•08643	2.3500
•03691	2.8600
•08740	2.8500
•08789	2.8600
•08838	2.8500
•08837	2.8600
•08936	2.8500
•08984	2.8600
•09033	2.8500
•09082	2.8505
•09131	2.8600
•091/0	2.8900
•09229	2.3600
•09277	2.8500
•09326	2.8500
• 09375	2.8500
•09424	2.8600
•09473	2.3600
•09521	2.8500
•09570	2.8600
•09619	2.3600
•09668	2.8400
•09717	2.8500
•09766	2.3500
•09814	2.8500
•09863	2.3500
•09912	2.8500



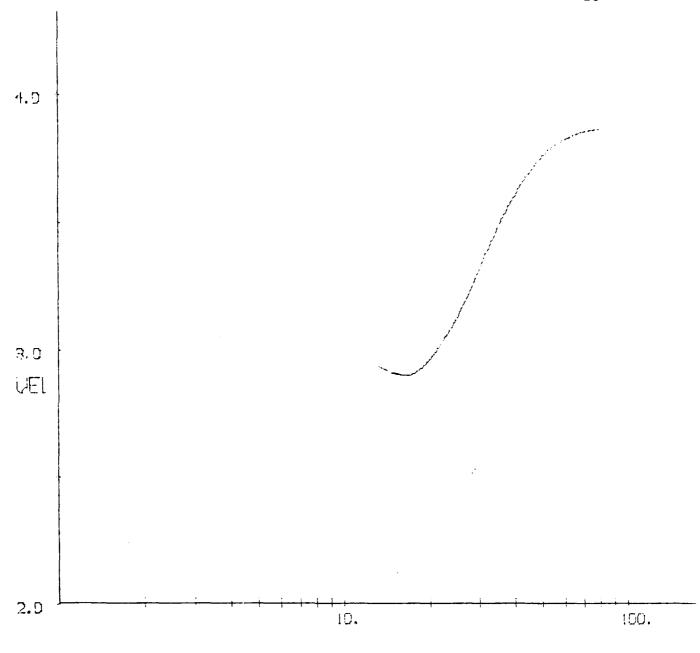
Rayleigh wave from a Novaya Zemlya explosion recorded at the Albuquerque, N. M., SRO. This signal was used to determine the phase-matched filter for the path Novaya Zemlya-Albuquerque.



100 SEC

Pseudo-autocorrelation function obtained by the application of the Novaya Zemlya-Albuquerque phase-matched filter to the Novaya Zemlya Rayleigh wave.





PERIOD

Plot of the apparent Rayleigh group velocity dispersion curve obtained for the Novaya Zemlya-Albuquerque path.

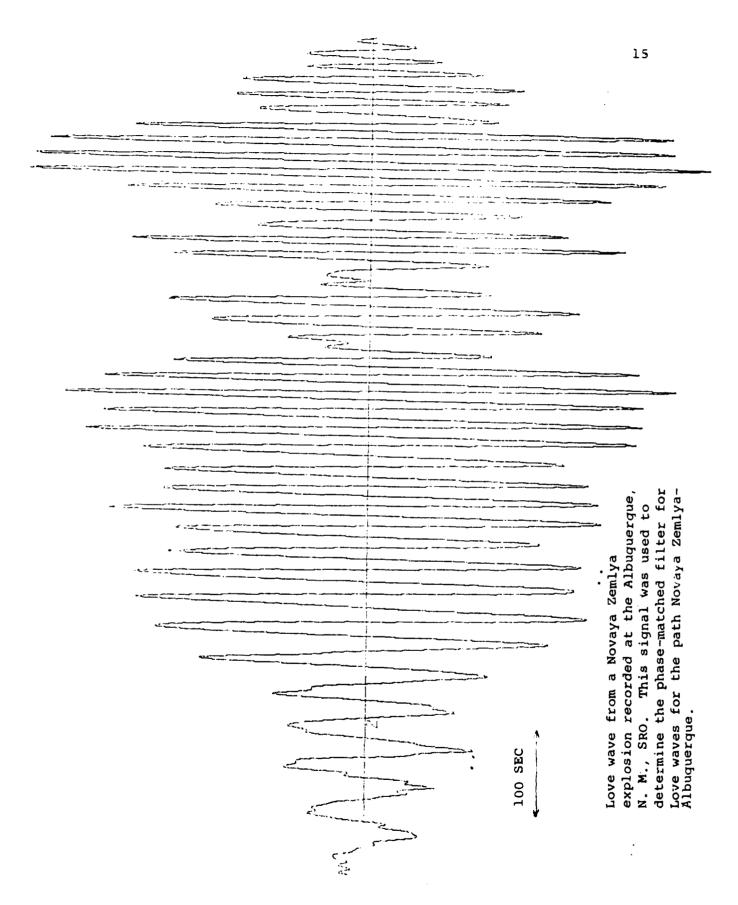
TABLED VALUES OF THE APPARENT RAYLEIGH GROUP VELOCITY DISPERSION CURVE FOR THE PATH NOVAYA ZEMLYA (73.35N, 55.08E) - ALBUQUERQUE, N. M., (34.93N, 106.45W)

# NOVAYA ZEMLYA (73.35N, 55.08E) - ALBUQUERQUE (34.93N, 106.45W) C = 0.500 cycles

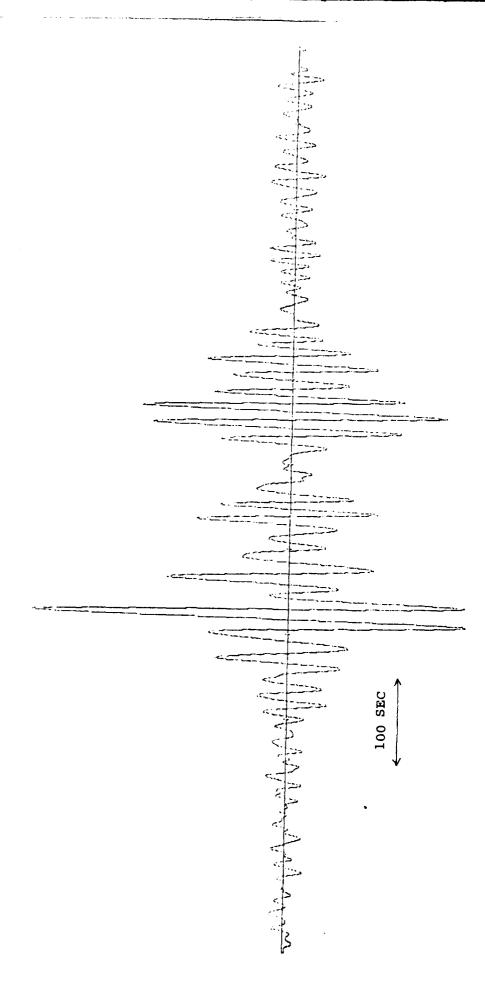
	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
	•00049	3.3898	24	
	•00098	3.9735	•02148	3.7264
	•00146	3.9536	•02197	3.7124
	•00195	3.9325	•02246	3.6980
	.00244	3.9217	•02295	3 • 6831
		3.9142	•02344	3.6579
	• 20342	3.9384	•02393	3 • 6524
	•00391	3.9040	•32441	3 • 6 3 6 5
	•00439	3.9007	•02490	3.6203
	•00433	3.8973	•02539	3.6038
	•00537	3.8942	•02588	3 • 5871
	•00536	3.3915	•02637	3.5702
	•00635	3.8393	•02636	3.5038
	•00634	3.8873	•02734	3.5362
	•00732	3.8353	•02783	3.5190
	•00781	3.8833	•05835	3.5018
	•00830	3.8315 -	•02881	3 • 4846
i			•02930	3.4574
	•00879	3.9797	•02979	3 • 4 5 0 3
	•00928	3.8781	•03027	3.4333
	•00977	3.8763	•03076	3.4164
	•01025	3.8759	•03125	3.3996
	•01074	3.8/50	•03174	3.3830
	•01123	3 • 8741	•03223	3.3564
	•01172	3.3730	•03271	3.3500
	•01221	3.3718	•03320	3.3338
	•31270	3.8/03	•03369	3.3177
	•01318	3.8584	•03418	3.3019
	•01367	3.8561	•03467	3.2861
	•01416	3.8633	•33516	3.2702
	•01465	3 • 8595	• 03564	3.2547
	•01514	3.3042	•03613	3.2.94
	• 01563	3.3432	•03662	3.2244
	•31611	3.8.15	•03711	3.2098
	•01660	3.3743	•03760	3 • 1 9 5 6
	•01709	3.8264	•03839	3.1317
	•01758	3.8179	•03857	3 - 1 584
	•01807	3.3787	•03936	3 • 1555
	•01855	3.7990	•03955	3.1432
	•01904	3.7886	•04004	3.1324
	•01953	3.1176	•04053	3.1221
	·02002	3.7556	•04102	3.1155
	•02051	3.7531	•04150	3-1027
	•02105	3.7%00	•04139	3.2735
			*04100	3-3/3/

	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
r	•04248	3.3846	•06641	2.9121
	•04297	3.0761	•06639	2.9126
	•04346	3.0678	•36738	5.3131
	•04395	3.0397	•06787	2.9136
	•04443	3.0519	•06836	2.9140
	•04492	3.0436	•06885	2.9145
	•04541	3.0354	•06934	2.9149
	•04590	3.0274	•06982	2.9148
	•04639	3.0196	•07031	2.9145
	•04638	3.0120	•07080	2.9142
	• 04736	3.0046	•07129	2.9140
	.04785	2.9374	•07173	5.9139
	·04834	2.9705	•07227	2.9139
	•04833	2.9333	•07275	2.9141
	•04932	2.9774	•0732+	2.9145
	•04950	2.9713	•07373	2.9152
	.05029	2.9555	•07422	2.9162
	·05078	2.9601	•07471	2.9181
	•05127	2 • 9343	•07520	2.9214
	•05176	2.9498	•07568	2.9250
	.05225	2 - 9 + 51	•07617	2.3583
	• 35273	2.9406	•07666	2.9328
1	·05322	2.9364	•07715	2.9369
1	•05371	2.9325	•07764	2.9410
	•05420	2.9288	•07813	2.9450
	.05469	2.9254	•07861	2.9491
	•05518	2.9224	•07910	2.3529
	• 35566	2.9196	•07959	2.9363
	•05615	2.9173	•08008	2.9583
	•05664	2.9147	•03037	2.9599
<b>—</b>	•05713	2.9127 -	- 08105	2.9514
	• 35762	2.9105	• 08154	2.9527
	• 05811	2.9093	•08233	2.9535
	• 25859	2.3079	•38232	2.9648
	•05938	2.9763	•08301	2.9657
	•05957	2.9561	•08350	2.9665
	• 36036	2.9758	.08398	2.9572
	•06055	2.905/	•08447	2.9679
	•06104	2.9)59	•08476	2.2690
	•06152	2.9061	• 38545	2.9702
	•06201	2.9165	•08594	2.9713
	•36250	2.9071	•08643	2.9723
- 4	•26299	2.7078	•08691	2.9734
	•06348	2.9785	•08740	2.9745
	•06396	2.9093	•03739	2.7755
	•36445	2.9101	•68836	2.3766
	•06494	2.9106	•08867	2.9775
	•06543	2.3111	•08936	2.9787
	•36592	2.9:13	•08984	2.9797

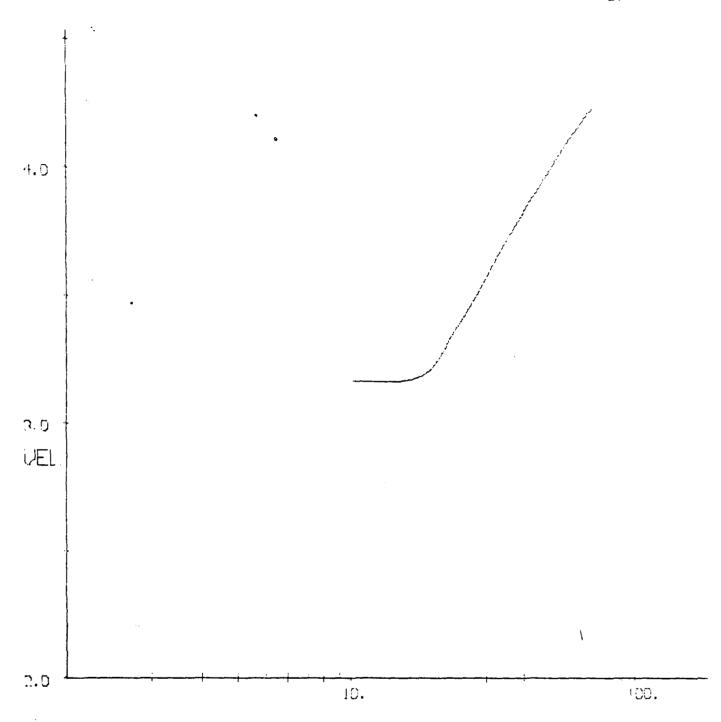
	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	
	•09033	2.9807	
	•09032	2.3317	The second of th
	•09131	2.3227	
	•09180	2.9337	
	•09229	2.9347	
1	•09217	2.9356	
	•09326	2.9866	
	• 39375	2.9375	
	•09424	2.9485	
	•09473	2 • 9894	
	•09521	5 • 3303	
	•09573	2.3915	
	•09619	2.9921	
	•09668	2.9930	
	•09717	5.333	
	•09766	2.9948	
	•09814	2.9956	
	. •09863	2.9965	
1	•09912	2.3373	



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Pseudo-autocorrelation function obtained by the application of the Novaya Zemlya-Albuquerque phase-matched filter to the Novaya Zemlya Love wave.



PERIOD

Plot of the apparent Love group velocity dispersion curve obtained for the Novaya Zemlya-Albuquerque path.

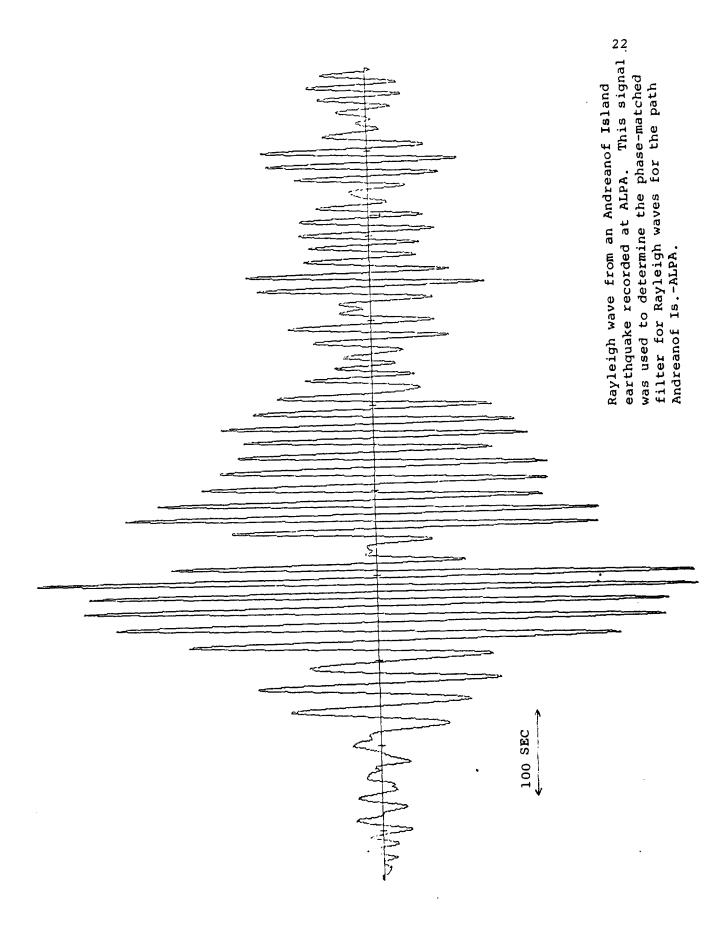
TABLED VALUES OF THE APPARENT LOVE GROUP VELOCITY DISPERSION CURVE FOR THE PATH NOVAYA ZEMLYA (73.35N, 55.08E) - ALBUQUERQUE, N. M. (34.93N, 106.45W)

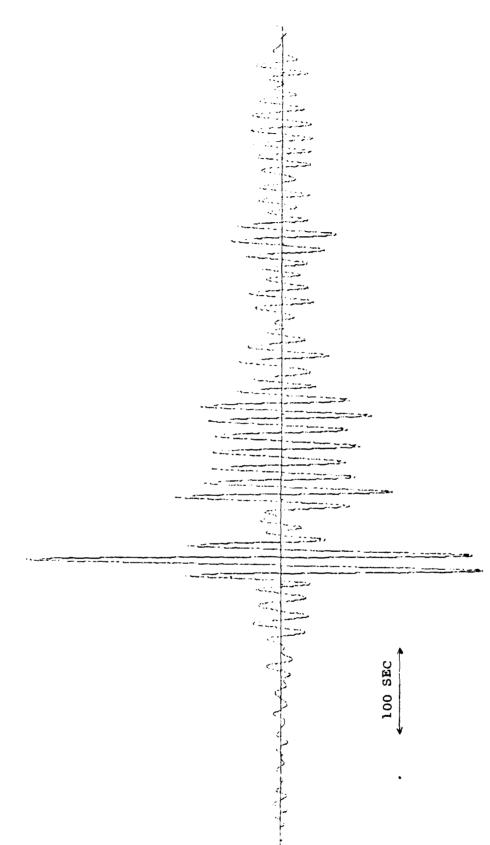
# NOVAYA ZEMLYA (73.35N. 55.08E) - ALBUQUERQUE (34.93N. 106.45W) C = +0.450 cycles

FREQUENCY (Hz)	LOVE GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	LOVE GROUP VELOCITY (KM/SEC)
•00049	4 • 5004	•02197	3.9235
•00098	4.5307	•02246	3.9064
•00146	4 • 5003	•02295	3.8895
•00195	4.5002	•02344	3.3729
•00244	4 • 4 7 6 6	•02393	3.8565
•00293	4.4717	•02441	3.8404
•00342	4.4364	•02490	3.8245
•00391	4 • 4305	•02539	3.8388
•30439	4 - 4745	•02588	3.7933
•00488	4 • 4703	•02637	3.7783
•00537	4 • 4666	•02636	3.7630
•00536	4 • 4525	•02734	3.7481
• 30635	4 • 4 5 7 9	•02783	3.7334
•00684	4 • 4523	•02832	3.7190
•00732	4 • 4 4 4 3	•02881	3.7047
•00781	4 • 4343	•02930	3.6905
•00830	4.4240	•02979	3.6766
•00879	4 • 4 1 2 1	•03027	3.6523
• 00928	4 • 3993	•03076	3.6497
•30977	4 • 3352	•03125	3.6357
•01025	4.3719	•03174	3.622+
•01074	4 • 3572	•03223	3.6093
•01123	4.3419	•03271	3.5963
•01172	4 • 3 ? 6 0	•03325	3.5335
•01221	4.3095	•03369	3.5709
•01270	4.2724	•03413	3.5584
•01318	4.2748	•03467	3.5460
•01367	4 • 2565	•03516	3.5335
•01416	4.2382	•03564	3.5213
•01455	4.2195	•03613	3.5092
•01514	4 • 1 78 3	•03662	3.4973
•01543	4 • 1783	•03711	3.4856
•01611	4.1376	•03760	3.4742
•01660	4 • 1 365	•03809	3.4331
•01709	4 • 1159	•33857	3.4522
•01758	4.0951	•03906	3.4415
•01807	4.0743	•03955	3.4313
•01855	4.0337	•04004	3.4221
•01904	4.0334	•04053	3.4132
•01953	4.0134	•04102	3.4045
•02002	3.9948	•04150	3.3960
•02031	3.9765	•04199	3.3876
•02100	3.3586	•0+2+8	3.3793
•02148	3.9407	•04297	3.3711

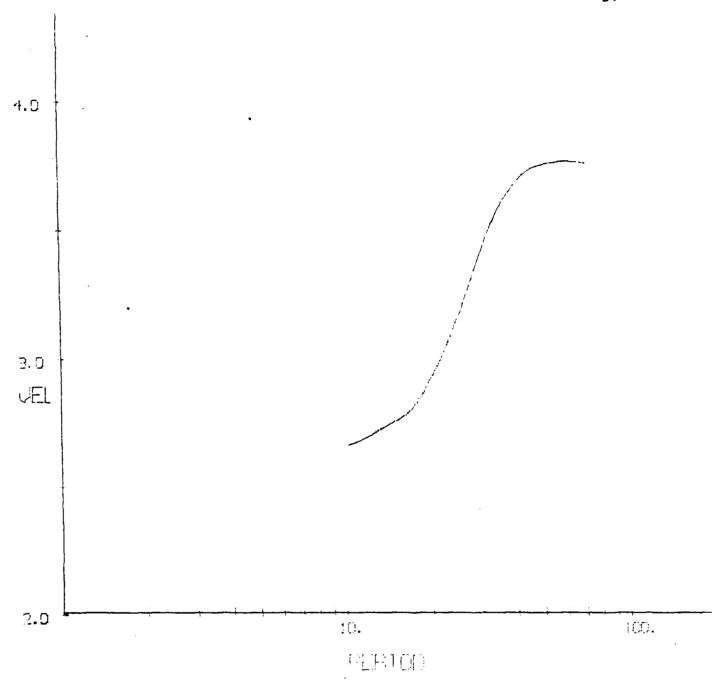
	FREQUENCY (Hz)	LOVE GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	LOVE GROUP VELOCITY (KM/SEC)
!	•04346	3.3528	•06738	3-1583
	•04395	3.3546	• 367 57	3.1642
	• 044+3	3.3463	•06836	3.1581
	•04492	3.3367	•06885	3.1680
	•04541	3.3263	•06934	3.1680
	•04590	3.3170	-06932	3.1680
	•04639	3.3072	•07031	3-1579
	•04683	3.2776	•07050	3.1579
	•04736	3.2382	•07129	3.1579
	•04735	3.2790	•07178	3-1579
	•04834	3.2700	•07227	3.1579
	•04833	3.2514	•07275	3.1579
	•04932	3.2532	-07324	3:1579
	•04960	3.2460	•07373	3.1580
	•05029	3.2397	-07422	3.1680
	•05073	3.2337	07471	3.1680
F	•05127	3.5585	•07520	
	•05176	3.5530	•07568	3 • 1680 3 • 1680
	•05225	3.2181	07617	3.1580
	-05273	3.2135	•07666	(2018 HOLDING 191 <b>8</b> ) (1919년) (2018년)
	• 35322	3.2095	•07715	3 • 1 5 8 0 3 • 1 5 8 0
	•05371	3.2057	•07764	3-15-5
	-05420	3.2021	•07813	
	•03469	3.1789	•07861	3.1680
	•05518	3.1961	•07910	3 • 1 5 8 0
• • • • • • •	-05566	3 • 1 7 3 5	•07959	3.1480
	•05615	3.1911	•03008	3 • 1680
	•05664	3.1490		3.1680
1	•05713	3-1871	•03057 •03105	3.1685
	•05762	3.1854		3 • 1 5 8 3
	•05811	3.1338	•0d154 •08233	3 • 1 5 8 0 3 • 1 5 8 0
· · · · · · · · · · · · · · · · · · ·	• 05859	3.1984	•08252	3.1680
	•05908	3 • 1 * 11	•08301	3.1580
1	• 35957	3-1798 -	•03350	
	• 36036	3.1785	•08398	3 · 1680 3 · 1680
	•06055	3.1772	•08447	
	•06104	3-1760	08496	3.1680
1	•06132	3.1747	그리고 그리고 있는데 그리고 있는데 그리고 있는데 그리고 있었다. 그는 경기를 위해 없는데 그리고 있다면 없는데 그리고 있다.	3.1535
	•06201	3 • 1739	•0\$545	3.1583
1	•06250	3 • 1730	•08534	3.1583
<b>.</b>	•06239	3.1721	•08643	3 • 1685
1	.06348	3.1714	• 03691	3 • 1680
1	•06396	3.1707	•08745	3.1680
	.06445	3-1761	•03749	3.1583
	•06494	3 • 1 5 9 5	•05838	3.1683
	• 36543	3.1592	•08837	3 • 1680
	•06592	3.1589	•08936	3 • 1580
	.06641	3.1585	•08934	3 • 1680
1	•06649	3-1994	•09033	3.1680
			•09032	3-1580

FREQUENCY (Hz)	GROUP VELOCITY (KM/SEC)
•09131	3.1580
•09130	3.1680
 •09229	3 • 1585
•09277	3 • 1680
•09326	3 • 1680
 •09375	3 - 1580
•09424	3.1680
•09473	3.1680
 •09521	3 • 1 5 8 0
•09570	3.1580
•09619	3 • 1580
 •09663	3.1685
•09717	3.1580
•09766	3.1680
•09814	3 • 1680
•09863	3 • 1680
•09912	3.1580





Pseudo-autocorrelation function obtained by the application of the Andreanof Is.-ALPA phase-matched filter to the Andreanof Island Rayleigh wave.



Plot of the apparent Rayleigh group velocity dispersion curve obtained for the Andreanof Is.-ALPA path.

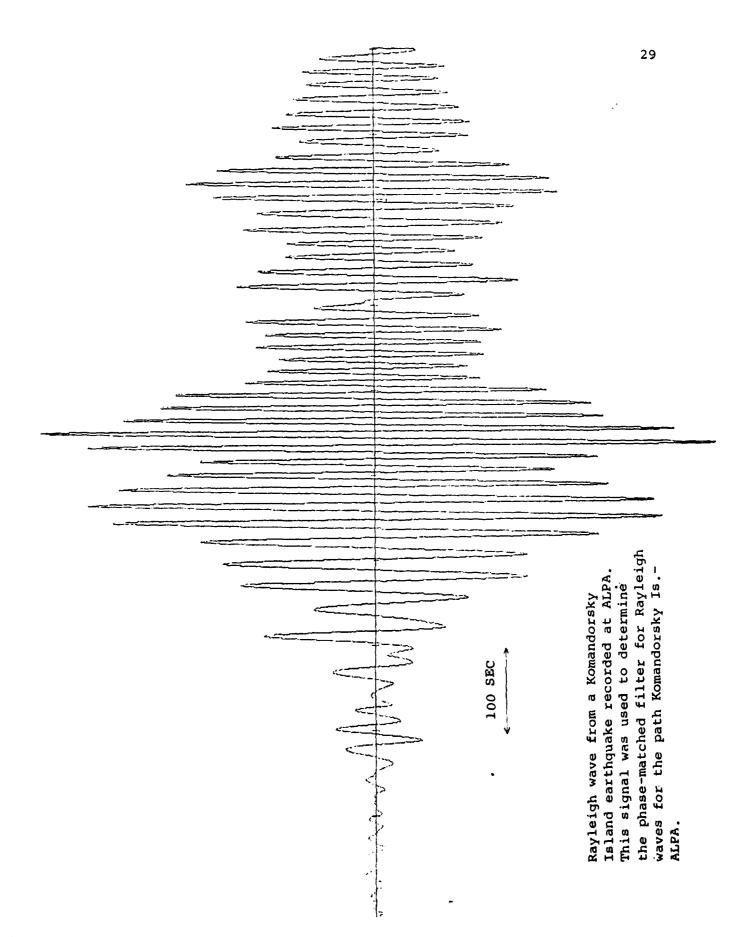
TABLED VALUES FOR THE APPARENT RAYLEIGH GROUP VELOCITY DISPERSION CURVE FOR THE PATH ANDREANOF ISLAND (51.60N, 173.50W) - ALPA (65.40N, 147.90W)

## ANDREANOF IS. (51.60N, 173.50W) - ALPA (65.40N, 147.90W) C = 0.0 cycles

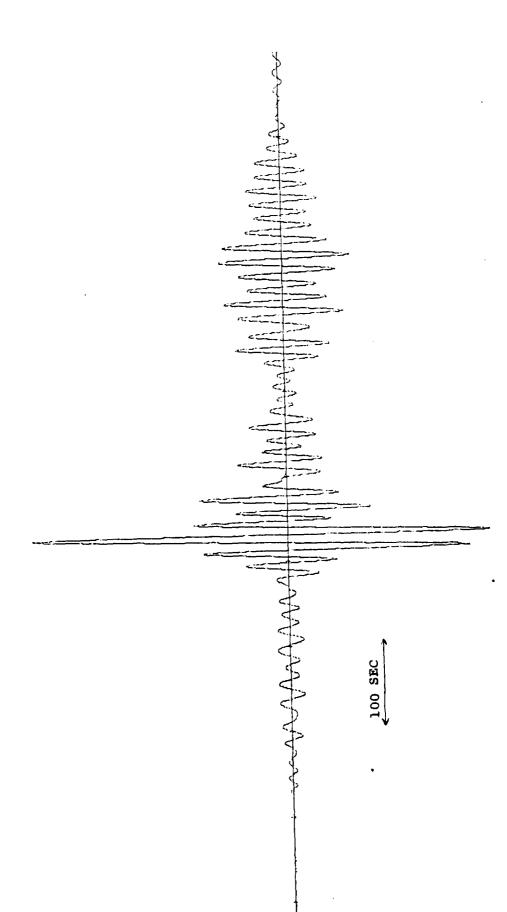
FREQUEN (HZ)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENC (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
• • • • • • • • • • • • • • • • • • • •	9 3.995	•02100	3.7387
•0009!	8 3.9151	•02148	3.7346
-30146	6 3.8010	•02197	3.7290
•00199	3 • 6 7 4 3	•02246	3.7221
•0024	4 3.6217	•02295	3.7141
.0029		- 02344	3 • 7051
•00342		•02393	3.6754
•0039	1 3.5352	•02441	3.6349
	3 • 5465	•02490	3.6742
• 30488	8 3.5592	•02539	3 • 6630
•00537	7 3.5715	•02588	3.6509
		•02637	3.6383
•0063	3 • 60 43	•02636	3.6250
•00634	4 3.6185	•02734	3.6112
•0073	3.6297	•02783	3.5967
•00733	-	26850.	3.5816
•0083		• 02851	3.5659
•00873	3 • 6690	•02930	3 • 5 + 97
• 3092		•02979	3.5330 3.5159
•0097	7 3.6364	• 03027	3.5159
•01025			3.4985
•0107		•03125	3.4309
•0112:	3 3.7131	•03174	3.4629
•0117	3.7227	.03223	3.4448
•0122		•03271	3.4265
•0127	0 3.7364	•03350	3.4079
•0131		•03369	3.3390
•0136	7 3.7442	•03418	3.3701
-01416		·C3467	3.3512
•0146	3 • 7504		3.3324
•0151	: [10] [10] [10] [10] [10] [10] [10] [10]	•03564	3.3137
•01563		•03613	3.2952
•0161	The second of th	•03662	3.2769
•0166		•03711	3.2584
•0170		•03760	3.2411
•0175		•03809	3.2236
•0180		•03857	3.2065
•0185		•03906	3.1898
•0190	[12] (12) (14) (14) (15) (15) (15) (15) (15) (15) (15) (15	•03955	3 • 1735
•0195		•04004	3.1585
•0800		•04053	3 • 1 4 3 8
•0205	3 • 7416	•//41.12	3.1295

FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	21
	3.•1155	•06494	2.7581	
•04199	3.1019	•06543	2.7558	
•04248	* 3.5387	• 06592	2.7537	-
•04297	3.0759	•06641	2.7316	
•04346	3.0633	•06669	2.7495	
•04395	3.0511	•06738	2.7476	
•04443	3.0392	•06787	2.7457	
•04492	3.0277	•06836	2.7439	
94536	3:8555		2.7421	
	2.9949	•06934	2.7404	
•04639 	2.9346	•06982	2 • 7387	
•04736	2.9744	•07031	2.7370	
•04735	2.9646	•07080 •07129	2 • 7353 2 • 7335	
	2.9548			
• • 04883	2.9454	•07178 •07227	2.7300	
•04932	2.9360	•07275	2.7382	
04930	2.9265	07324		
•05029	2.9169	•07373	2 • 7245	
•05078	2.9075	•07422	2.7232	
	2.8984	•07471	2.7216	
•05176	2.8393	•0/520	2.7200	
•05225	2.8905	•07568	2.7185	
	2.3721	•07617	2.7170	
•05322	2.8638	•07656	2.7155	
•05371	2.8557	•07715	2.7139	
-05420	.2.8480		2.7123	
•03469	2.8405	•07813	2.7109	
• 05518	2.8336	•07861	2.7093	
	2.8276	•07910	2.7078	
•05615	5.8550	•07959	2.7563	
•05664	2.8167	80080	2.7048	
	2.8117	•08057	2.7032	
•05762	2.8069	•0*105	2.7016	
•05811	2.8323	•08154	2.7001	
05859	2.7981	•08203	2.6985	
•05908	2.7940	•08252	2.6967	
•05957	2.7902	•08301	2 • 6950	
•06006	2.7865	•08350	2.6935	
•06055	2.7831	•08398	2.6865	
•06104	2.7798	•08447	2.6251	
	2.7767	•08436	2.6537	
•06201	2.7738	•08545	2.6324	
•06250	2.7708	•08534	2.6810	
-06299	2.7681	•08643	2.6797	
•06348	2.7554	•08631	2.6724	
•06396	2.7529	•08740 •08789	2.6772	
L	2.7505	•00/03	2.6760	

· FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
•08838 •08837	• 2 • 6748
•08936	2 • 6735 2 • 6725
• 08984	2.6713
•09033	2.6702
•09082	2.6691
•09180 •09229	2 • 6670 2 • 6660
•09277 •09326	2 • 6 6 4 0 2 • 6 6 4 0
•09375	2.6030
	2.6621 2.6612
•09521	2•6603 _ 2•6594
•09619	2.6585
•03668	2.6577
•09717	2.6568
•09766	2.6560
•09814	2 • 6 5 5 2
•09863 •09912	2 • 6544 2 • 6536

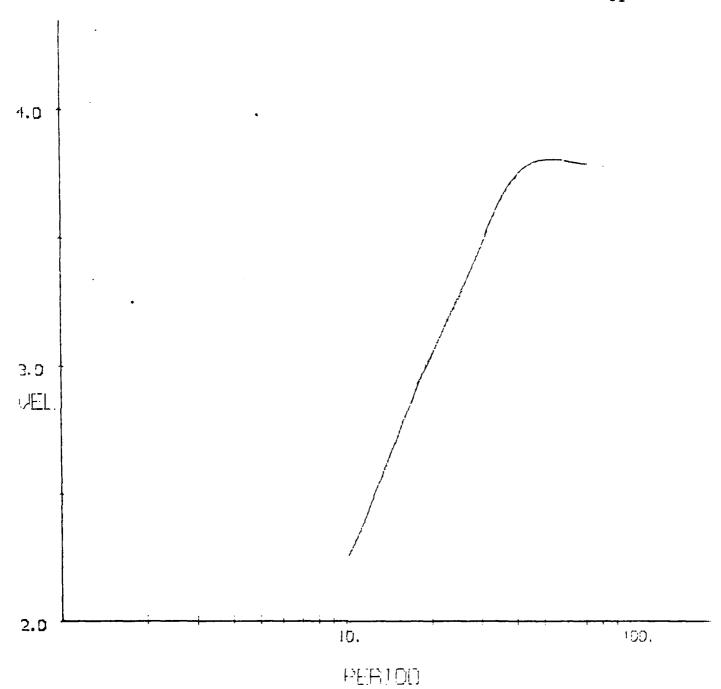


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pseudo-autocorrelation function obtained by the application of the Komandorsky Is.-ALPA phase-matched filter to the Komandorsky Island Rayleigh wave.

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Plot of the apparent Rayleigh group velocity dispersion curve obtained for the Komandorsky Is.-ALPA path.

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TABLED VALUES FOR THE APPARENT RAYLEIGH GROUP VELOCITY DISPERSION CURVE FOR THE PATH KOMANDORSKY ISLAND (54.40N, 167.5E)-ALPA (65.03N, 147.20W).

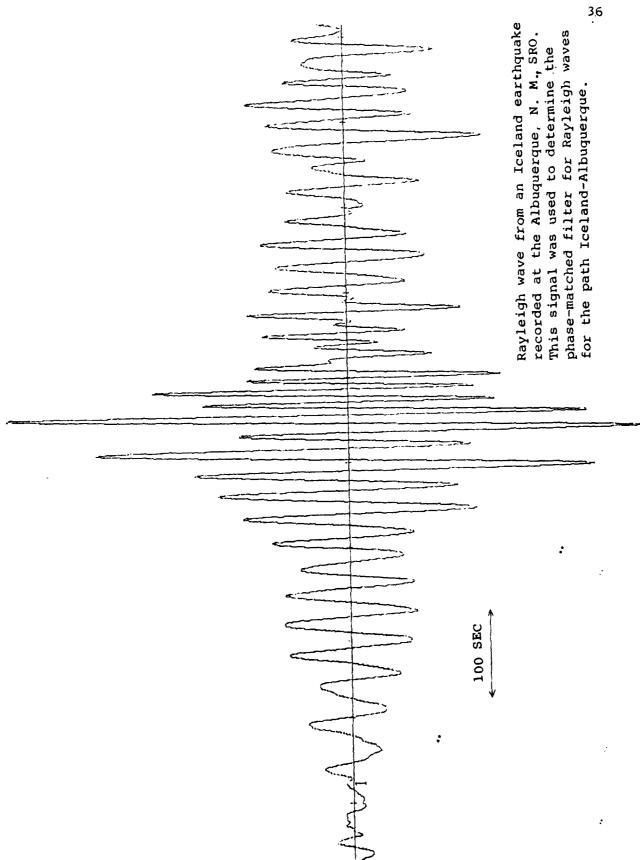
#### KOMANDORSKY IS. (54.40N, 167.50E) - ALPA (65.03N, 147.20W)

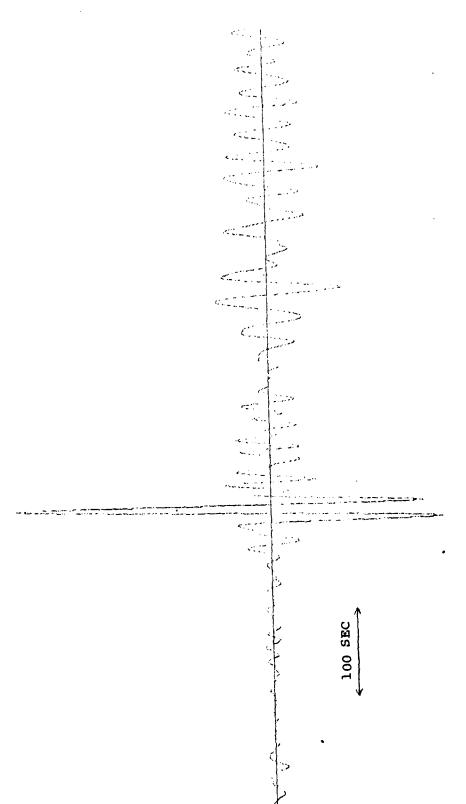
#### C = +0.425 cycles

	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
	•00049	3.9301	•02148	3.7942
	•00038	3.9932	•02197	3.7398
	.00146	3.9502	•02246	3.7541
	•00195	3.3082	•02295	3.7775
	.00244	3.7015	•02344	3.7700
	•00293	3.6324	•02393	3.7614
	•00342	3.5992	•02441	3.7519
-	•00391	3.5350	•02430	3 • 7 • 15
	•00439	3.5727	•02539	3.7304
	•00488	3-6101	.02568	3.7182
	•00537	3.6308	•02637	3.7055
	•00586	3 • 6 + 6 9	•02686	3.6919
	•00635	3.6617	.02734	3.6779
	•03664	3.6771	•02763	3.6531
	•00732	3.6233	•02832	3 • 6 4 7 7
	-00781	3.7762	•02881	3.6316
	•00830	3.7163	•02930	3.6151
	•00879	3.7267	•02979	3.5982
	•00928	3.7383	•03027	3.5311
	•00977	3 • 7 4 7 7	•03076	3.5637
	•01025	3 • 7545	•03125	3.5462
	•01074	3.7502		3.5285
	•01123	- 3.7554	•03223	3.5108
	•01172	3.7698	•03271	3.4932
	•01221	3.7737		3 • 4759
	•01270	3.7771	•03359	3 • 4588
	•01318	3.7302	•03418	3 • 4 4 1 5
	•01367	3.7327	•03467	3 • 4251
	.01416	3.7848	•03516	3 • 4086
	•01465	3.7868	•03564	3.3982
	-01514	3.7889	•03613	3.3762
	• 01563	3.7915	•03662	3.3605
	•31611	3.7949	•03711	3.3450
	•01660	3.7979	•03760	3.3299
	•01709	3.8007	•03809	3.3152
	•01758	3.8028	•03857	3.3008
	•01807	3.8039	•03906	3.5864
	•01855	"3.8040"	•03955	3.2733
	•01904	3.8735	•04004	3.2511
,	•01953	3.8)24	•04053	3.2493
1	-02005	3.8014	•04102	3.2377
	•02051	3.7998	•04150	3.2264
	•02100	3.7974	•04199	3.2153

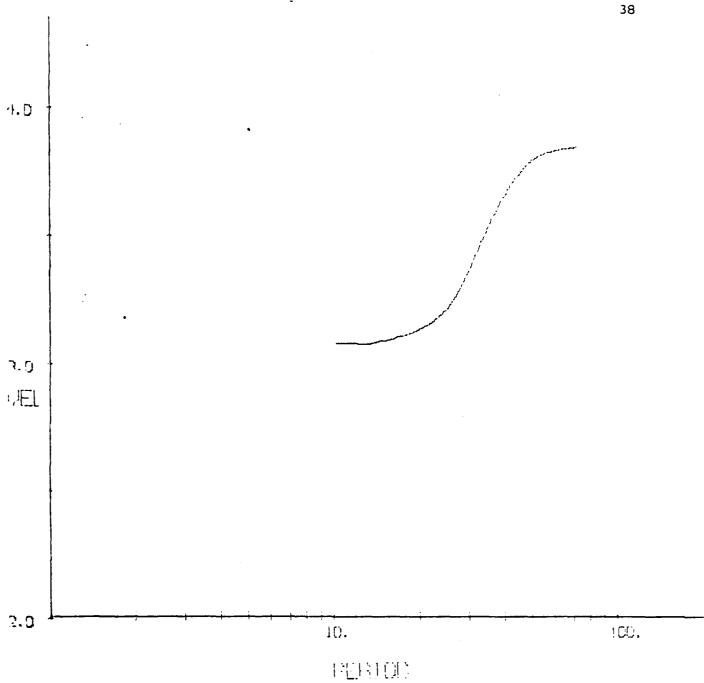
	FREQUENCY	RAYLEIGH	FREQUENCY	RAYLEIGH
	(Hz)	GROUP	(Hz)	GROUP
	<del></del>	VELOCITY		VELOCITY
		(KM/SEC)		(KM/SEC)
		TRM/SEC)		
	·04248	3 • 2045	•06641	2.7165
	•04297	3 • 1939	•06639	2.7566
•	•04346	3 • 1 5 3 3	•06738	2.6967
	•04335	3.1730	•06757	2.6370
	•04443	3 • 1628	•06836	2.6774
	•04492	3 • 1525	•06865	2.6573
	•04541	3 • 1 4 1 7	•06934	2 • 6585
	• 3 4 5 9 0	3 • 1 3 1 0	- 36962	2.6494
	•04639	3.1503	•07031	2.6404
	•04688	3.1098	•07030	2.6315
	•04736	3.0993	•07129	2.6233
	·04745	3.0391	•07173	2.6145
	•04834	3.0791	•07227	2.6065
	•04863	3.0692	•07275	2.5785
	-04932	3.0594	•07324	2.5903
	•04980	3.0505	•07373	2.5333
	•05029	3.0488	•07422	2.5759
	•05078	3.0341	•07471	2.5687
	.05127	3.0261	•07520	2.5617
	•05176	3.0181	•07568	2.5342
	•05225	3.0102	•07617	2.5540
	•05273	3.0023	•07666	2 • 5 4 6 4
	•05322	2.9943	•07715	2.5385
	•05371	2 • 9363	•07764	2.5309
	.05420	2.9781	•0/813	2 • 5 2 3 1
	•05469	2.9699	•07861	2.5154
	03518	2.9612	•07910	2.5)77
	.05566	2.9513	•07959	2.5001
	•05615	2.9412	•03008	2.4324
<del> </del>	• 35664	2.9309	•08057	2.4348
	•05713	5.9204	•08105	2.4773
	•05762	2.9793	•08154	2 • 4593
	-05811	2.8390	•03203	2.4623
	.05859	2.8381	•08252	2 • 4549
	.05908	2.8771	-08301	2.4475
	• 35957	2.3560	•08350	2.4402
	•06006	2.8548	•08398	2 • 4329
	•C6055	2.3435	•08447	2 • 4257
•••••••••	.06104	2.8324	•08496	2 • 4185
	•06152	2.8211	•08545	2 • 4114
	•06201	2.8099	•08574	2.4544
•	06250	~ 2.7393	•08643	2 • 3975
	•06233	2.7857	•03691	2.3906
	•06348	2.7782	•08740	5.3833
· · · · · · · · · · · · · · · · · · ·	• 36376	2.7678	•08739	2.3772
1	.06445	2.757+	•08838	2.3705
1	.36494	2.7471	•03837	2.3541
	•065+3	2.7363	•08936	2.3577
	•065/2	2.7265	•03934	2 - 3514

FREQUENC (Hz)	Y RAYLEIGH GROUP VELOCITY (KM/SEC)
•09033	2.3451
•09082 •09131	2 • 3393 2 • 3335
•09130	5.3580
•03229	2 • 3225
•09277	2.3171
•07326 •09375	2·3118 2·3065
•09424	2.3014
•09473	2.2363
•09521	2.2913
•09570	2.2364
•09619	2.2315
•09668	2.2767
•09717	2.2720
•07765	2.2573
•09814	2.2527
•09863	2.2536





Pseudo-autocorrelation function obtained by the application of the Iceland-Albuquerque phase-matched filter to the Iceland Rayleigh wave.



Plot of the apparent Rayleigh group velocity dispersion curve obtained for the Iceland-Albuquerque path.

TABLED VALUES FOR THE APPARENT RAYLEIGH GROUP VELOCITY DISPERSION CURVE FOR THE PATH ICELAND (66.05N, 16.69W) - ALBUQUERQUE (34.93N, 106.45W).

### ICELAND (66.05N, 16.69W) - ALBUQUERQUE (34.93N, 106.45W) C = -0.180 cycles

	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (HZ)	RAYLEIGH GROUP VELOCITY (KM/SEC)
	•00049	3.9953	•02100	3.7315
	•10018	3.9883	•02148	3.7599
	•33146	3.9795	•02197	3.7577
	•00195	3.9693	•02246	3.7448
	•00244	3.9610	•02295	3.7313
	•00533	3.9535	•02344	3.7172
	•30342	3.9454	•02393	3.7026
	•00391	3.9173	•32441	3 • 637 5
	• 00439	3.9307	•32490	3.6715
	•00488	3.9241	•02539	3 • 6553
i	•00537	3.9180	•02538	3.6386
•	•00586	3.0153	• 52637	3.6716
	•00635	3.9069	•08686	3.6045
	•30684	3.9018	•02734	3.5371
· · · · · · · · · · · · · · · · · · ·	00732	3.8970	•02783	3.5697
•	•00731	3.8925	•02832	3.5522
	•00830	3-8884	•02831	3.5347
	-00879	3.8544	•02930	3.5172
	•00928	3.8507	•02979	3.4997
	•00977	3.8/73	•03027	3.4824
	•01025	3.8741	•03076	3.4652
l .	•01074	3.3/12	•03125	3 • 4 + 8 3
	•01123	3.8683	•03174	3.4316
	•01172	-3.8555	•03553	3.4152
	•01221	3.8530	•03271	3.3792
	•01270	3.8403	•03350	3 • 3835
	•01318	3.8575	•03369	3.3685
	•01367	3.8552	•03418	3.3534
	•01416	3.8526	•03467	3.3392
	•01465	3.8501	•53516	3:3553
	·G1514	3.3481	•03564	3.3129
	•01563	3 • 8 • 5 %	•03613	3.3006
	•31611	3.8434	•03662	3.2387
	•01660	3.8.05	•03711	3.2774
	•01739	3.8372	•03760	3.2565
	•31758	3.8334	•03809	3.2763
	•01807	3.829	•03857	3.2466
	•01855	3.824)	•03906	3.2374
	•31934	3.5182	•03955	3.5583
	•01953	3.8116	•04034	3.2215
	•02002	3.8023	•04053	3.2147
	•08051	3.7973	•04102	3.235

FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)
• 34150	3.2026	•06396	3.0976
•04199	3 • 1 371	•06445	3.0764
.04248	3 • 1721	•06494	3.0957
•04297	3 • 1 8 7 3	•06543	3.0352
•04346	3-1329	•06592	3.0947
•04375	3.1788	•06641	3.0942
•04443	3-1/50	•06639	3.0938
•04492	3.1712	•06735	3.0734
	3 • 1 5 7 5	•06787	3.0330
•04590	3-1541	• 06836	3.0925
•04639	3-1508		3.0351
•34633	3.1377	• 56934	3.0917
• 247.36	3 - 1545	•06982	3.0909
•04735	3.1520	•07031	3 • 2433
• 348.44	3.1.93	•07030	3.0383
	3.1.67	•07129	3.0877
•04932	3.1+43	•07178	3.0867
•04930	3 - 1 + 17	•07227	3.0856
•05029	3 • 1 3 9 1	•07275	3.0846
•05078	3 - 1 36.5	•07324	3.0836
•05127	3.1342	•073/3	3.0325
•05176	3.1319	•07422	3.0517
05225	3.1297	•07471	3.0310
• 25273	3-1275	•07520	3.0305
•05322	3.1250	•07568	3.0405
• 25371	3.1236	•37617	3.0799
	3.1218	•07656	3.0795
• 25469	3.1202	•07715	3.0795
• 35518	3-1189	•37764	3.0794
• 25566	3.1177	•07813	3.0793
• 05615	3.1167	•07861	3.0724
•35654	3 - 1156	•07913	3.3794
•05713	3-1145	•37959	3.0795
•03762	3.1137	•03008	3.079
• 05811	3-1128	•08057	3.0%00 .
	3.111"	•08105	3.0%04
•05908	3.11.7	•08154	3.0507
•35957	3.1199	•08203	3.0710
	3-1785-	.08252	3.0314
•06055	3 • 1 ) 7 1	•08301	3.0317
•36134	3.1057	• 08350	3.0×51
• 76152	3+1742	•08338	3.0324
•06201	3 • 102×	•03447	3.0327
•36293	3-1015	•08436	3.0358
· •06299	3.1001	•03545	3.0:25
• 763+8	3.0988	•03534	3.048)

	FREQUENCY (Hz)	RAYLEIGH GROUP VELOCITY (KM/SEC)		
· —	•03643	3.0329		
	• 08691	3.0329		
	•087+3	3.0329		
<b> -</b>	• 28789	3.0329		
i	• 28838	3.0323		
	•08837	3.0328		
	08936	3.0327		· · · · · · · · · · · · · · · · · · ·
	•08984	3.0327		
	•09033	3.0827		
	-03025	3.0327		
	• 09131	3.2327		
-1	•69130	3.0327		
		3.0327		· · · · · · · · · · · · · · · · · · ·
	•09277	3.0327		
	•09326	3.0327		
<del>-</del>	-·····································	3.3427	•	and the second second second second second
	•09424	3.0427		
	•09473	3.0327		
		3.0027	······	
	•09570	3.0327		
i	•09619	3.0327		
•	•09668	3.0527	* * * * * * * * * * * * * * * * * * * *	
	•03717	3.3.27		
	•09766	3.3527		
	•07814	3.0327		·- ·- ·-
1	•09863	3.7327		
	•09912	3.0327		